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PATENT APPLICATION

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re the Application of

Edwin Stephen TWIGG

Application No.: NEW U.S. SECURITY APPLICATION

Filed: June 3, 1998

Docket No.: 100745

For: A FIBRE REINFORCED METAL ROTOR

CLAIM FOR PRIORITY (MULTIPLE)

Assistant Commissioner for Patents  
Washington, D.C. 20231

Sir:

The benefit of the filing dates of the following prior foreign applications filed in the following foreign country(ies) is hereby requested for the above-identified patent application and the priority provided in 35 U.S.C. §119 is hereby claimed:

U.K. Patent Application No. 9711768.3, filed June 3, 1997

U.K. Patent Application No. 9711771.7, filed June 5, 1997

In support of this claim, certified copies of said original foreign applications:

  X   are filed herewith.

           were filed on            in Parent Application No.            filed           .

It is requested that the file of this application be marked to indicate that the requirements of 35 U.S.C. §119 have been fulfilled and that the Patent and Trademark Office kindly acknowledge receipt of these documents.

Respectfully submitted,

  
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the undersigned, being an officer duly authorised in accordance with Section 74(1) and (4) of the Deregulation & Contracting Out Act 1994, to sign and issue certificates on behalf of the Comptroller-General, hereby certify that annexed hereto is a true copy of the documents as originally filed in connection with the patent application identified therein.

further certify that pursuant to Section 22(1) of the Patents Act, 1977, the Comptroller has ordered prohibition of publication of the said specification.

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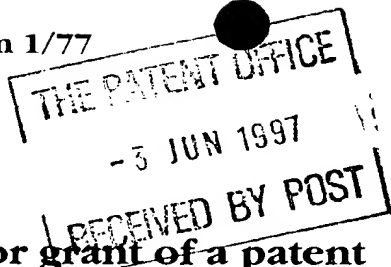
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P01/7700 25.00 - 9711768.3

# Request for grant of a patent

(See the notes on the back of this form. You can also get an explanatory leaflet from the Patent Office to help you fill in this form)

The Patent Office

Cardiff Road  
Newport  
Gwent NP9 1RH

1. Your reference

DY 2580

2. Patent application number

(The Patent Office will fill in this part)

9711768-3

- 3 JUN 1997

3. Full name, address and postcode of the or of each applicant (*underline all surnames*)

ROLLS-ROYCE plc  
65 BUCKINGHAM GATE  
LONDON SW1E 6AT

Patents ADP number (*if you know it*)

00003970002

If the applicant is a corporate body, give the country/state of its incorporation

ENGLAND

4. Title of the invention

A FIBRE REINFORCED METAL ROTOR

5. Name of your agent (*if you have one*)

M A GUNN

"Address for service" in the United Kingdom to which all correspondence should be sent (*including the postcode*)

ROLLS-ROYCE plc  
PATENTS DEPARTMENT  
PO BOX 31  
DERBY DE24 8BJ

Patents ADP number (*if you know it*)

6. If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or of each of these earlier applications and (*if you know it*) the or each application number

Country

Priority application number  
(*if you know it*)

Date of filing  
(*day / month / year*)

7. If this application is divided or otherwise derived from an earlier UK application, give the number and the filing date of the earlier application

Number of earlier application

Date of filing  
(*day / month / year*)

8. Is a statement of inventorship and of right to grant of a patent required in support of this request? (*Answer 'Yes' if:*

YES

- a) any applicant named in part 3 is not an inventor, or
  - b) there is an inventor who is not named as an applicant, or
  - c) any named applicant is a corporate body.
- See note (d))

# Patents Form 1/77

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Continuation sheets of this form

Description	10
Claim(s)	2
Abstract	1
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Priority documents

Translations of priority documents

Statement of inventorship and right to grant of a patent (*Patents Form 7/77*) 2

Request for preliminary examination and search (*Patents Form 9/77*) 1

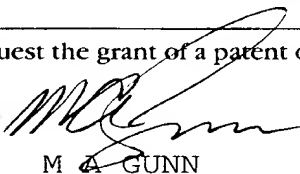
Request for substantive examination (*Patents Form 10/77*) 1

Any other documents  
(please specify)

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11. I/We request the grant of a patent on the basis of this application.

Signature



Date

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12. Name and daytime telephone number of person to contact in the United Kingdom

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## Warning

*After an application for a patent has been filed, the Comptroller of the Patent Office will consider whether publication or communication of the invention should be prohibited or restricted under Section 22 of the Patents Act 1977. You will be informed if it is necessary to prohibit or restrict your invention in this way. Furthermore, if you live in the United Kingdom, Section 23 of the Patents Act 1977 stops you from applying for a patent abroad without first getting written permission from the Patent Office unless an application has been filed at least 6 weeks beforehand in the United Kingdom for a patent for the same invention and either no direction prohibiting publication or communication has been given, or any such direction has been revoked.*

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3 JUN 1997

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right to grant of a patent**

The Patent Office

Cardiff Road  
Newport  
Gwent NP9 1RH

1. Your reference

DY 2580

2. Patent application number

(if you know it)

9711768-3

3. Full name of the or of each applicant

ROLLS-ROYCE plc

4. Title of the invention

A FIBRE REINFORCED METAL ROTOR

5. State how the applicant(s) derived the right  
from the inventor(s) to be granted a patent

BY VIRTUE OF SECTION 39(1) (a) OF THE PATENTS ACT 1977

6. How many, if any, additional Patents Forms

7/77 are attached to this form?

1

(see note (c))

7.

I/We believe that the person(s) named over the page (and on  
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which the above patent application relates to.

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Enter the full names, addresses and postcodes of the inventors in the boxes and underline the surnames

EDWIN STEPHEN TWIGG  
1 TELFORD CLOSE  
MICKLEOVER  
DERBY  
DE3 5NU

Patents ADP number *(if you know it):*

Patents ADP number *(if you know it):*

Patents ADP number *(if you know it):*

**Reminder**

**Have you signed the form?**



A FIBRE REINFORCED METAL ROTOR

The present invention relates to a fibre reinforced metal rotor. The present invention relates particularly to fibre reinforced metal discs and fibre reinforced metal rings which are suitable for use in gas turbine engines as blade carrying compressor, or turbine, rotors. The present invention is particularly suitable for applications where the fibre reinforced metal rotor has a large diameter and is intended to rotate at high speeds.

A conventional compressor rotor for a gas turbine engine comprises a solid unreinforced metal disc which has a relatively large hub, a relatively large rim and a relatively thin diaphragm which extends between the hub and the rim. The rim carries compressor blades which extend radially from the rim. The compressor blades may be integral with the rim or the compressor blades may have roots which are arranged to locate in axially or circumferentially extending grooves in the rim. The compressor blades which are integral with the rim may be friction welded to the rim or may be machined from the forged disc.

It is known to provide a compressor rotor for a gas turbine engine which comprises a solid fibre reinforced metal ring, for example as in UK Patent GB2247492. The ring carries compressor blades which extend radially from the ring. The compressor blades may be integral with the ring or the compressor blades may have roots which are arranged to locate in axially or circumferentially extending grooves in the ring. The compressor blades which are integral with the ring may be friction welded to the ring or may be machined from the ring. This solid fibre reinforced compressor rotor

does not have a diaphragm and hub as in the conventional solid metal compressor disc.

It is important in gas turbine engines used on aircraft to minimise the weight of the gas turbine engine. It is also necessary to increase the thrust of gas turbine engines, and this has necessitated an increase in the size of the gas turbine engine. It has been found that the use of solid fibre reinforced metal rings, about 0.5 metre outer radius, designed to operate at a rotational speed of about 11000 revolutions per minute (rpm) and carrying large, heavy, blades are about 10 percent heavier than a conventional solid metal disc. This is because the fibre reinforced metal ring has to be made massive enough to carry the loads of the blades.

The present invention seeks to provide a solid fibre reinforced metal rotor which has reduced weight compared to the known solid fibre reinforced metal ring and known solid metal disc.

Accordingly the present invention provides a fibre reinforced metal rotor comprising at least two rings of fibres, the fibre reinforced metal rotor having an axis of rotation, a first ring of fibres being arranged substantially at a first radial distance from the axis of rotation, a second ring of fibres being arranged substantially at a second radial distance from the axis of rotation and the second radial distance is greater than the first radial distance.

Preferably the fibre reinforced metal rotor comprises a disc, the disc comprising a hub, a rim and a diaphragm extending radially between the hub and the rim.

Preferably the first ring of fibres is arranged in the hub and the second ring of fibres is arranged in the rim.

The fibre reinforced metal rotor may comprise titanium, titanium aluminide, an alloy of titanium, or any suitable metal, alloy or intermetallic which is capable of being bonded.

5 The reinforcing fibres may be silicon carbide, silicon nitride, boron, alumina or other suitable fibres.

The fibre reinforced metal rotor may have at least one rotor blade. The at least one rotor blade may be integral with the fibre reinforced metal rotor. The at least one  
10 rotor blade may have a root arranged to fit in at least one axially, or circumferentially, extending groove in the fibre reinforced metal rotor.

The fibre reinforced metal rotor has an outer radius, the outer radius is at least about 0.5 metres.

15 The present invention will be more fully described by way of example with reference to the accompanying drawings, in which:-

Figure 1 is a cross-sectional view through a conventional solid unreinforced metal rotor.

20 Figure 2 is a cross-sectional view through a known fibre reinforced metal rotor.

Figure 3 is a cross-sectional view through a fibre reinforced metal rotor according to the present invention.

Figure 4 is a cross-sectional view through a gas turbine  
25 engine showing a fibre reinforced titanium compressor rotor.

Figure 5 is a cross-sectional view through a preform used to make a fibre reinforced metal rotor as shown in figure 3.

A conventional compressor rotor 10, as shown in figure  
30 1, for a gas turbine engine comprises a solid unreinforced metal disc 12 which has a relatively large hub 14, a relatively large rim 16 and a relatively thin diaphragm 18

which extends between and interconnects the hub 14 and the rim 16. The rim 16 carries compressor rotor blades 20 which extend radially from the rim 16. The compressor rotor blades 20 may be integral with the rim 16 or the compressor rotor blades 20 may have roots which are arranged to locate in axially or circumferentially extending grooves, not shown, in the rim 16. The compressor rotor blades 20 which are integral with the rim 16 may be friction welded to the rim 16 or may be machined from the forged disc.

Another known compressor rotor 30, as shown in figure 2, for a gas turbine engine comprises a ceramic fibre reinforced metal ring 32. The ring 32 carries compressor rotor blades 34 which extend radially from the ring 32. The ring 32 comprises a ring of fibres 36, the individual ceramic fibres 38 extending circumferentially through 360 degrees. The compressor rotor blades 34 may be integral with the ring 32 or the compressor rotor blades 34 may have roots which are arranged to locate in axially or circumferentially extending grooves in the ring 32. The compressor blades which are integral with the ring 32 may be friction welded to the ring 32 or may be machined from the ring 32.

It is to be noted that the ceramic fibre reinforced compressor rotor 30 does not have a diaphragm and hub as in the conventional solid metal compressor disc 10. The ring of fibres 38 increases the hoop strength of the ring 32 and the ceramic fibres 38 reduce the density of the ring 32. The volume fraction of fibres in the ring of fibres 38 is about 30 percent.

As an example a ceramic fibre reinforced compressor rotor 30 with an outer radius of 0.5 metres, or greater, carrying large, heavy, compressor blades and arranged to operate at about 11000 revolutions per minute (rpm) is

heavier than a conventional solid metal compressor rotor 10 with the same diameter. This is because the free ring radius, the radius beyond which the material of the rotor is not load bearing, decreases with increasing speed of rotation. The free ring radius for a ceramic fibre reinforced ring 32 operating at 11000 rpm is very close to the outer radius of the ceramic fibre reinforced ring 32. Therefore the ceramic fibre reinforced metal ring 32 has to be more massive to carry the loads of the compressor blades 34. The introduction of the ceramic fibres 38 reduces the density of the ring 32, but does not reduce the weight of the ring 32 to less than that of the ring 10, because the mass of the ring 32 is concentrated substantially at the radius of attachment of the blades 34 to the ring 32.

However, the free ring radius decreases with increasing speed and decreases with increasing blade loading. The free ring radius is also dependent upon the metal and the fibres. The free ring radius for a fibre reinforced metal is greater than that for an unreinforced metal. Thus a ceramic fibre reinforced compressor rotor 32 with an outer diameter less than 0.5 metres may be heavier than a conventional solid metal compressor rotor 10, of the same diameter, if the speed of rotation and or blade loads are sufficiently high.

A compressor rotor 40 according to the present invention, as shown in figure 3, for a gas turbine engine comprises a ceramic fibre reinforced metal disc 42 which has a relatively large hub 44, a relatively large rim 46 and a relatively thin diaphragm 48 which extends between and interconnects the hub 44 and the rim 46. The rim 46 carries compressor rotor blades 50 which extend radially from the rim 46. The compressor rotor blades 50 may be integral with the rim 46 or the compressor rotor blades 50 may have roots which

are arranged to locate in axially or circumferentially extending grooves, not shown, in the rim 46. The compressor rotor blades 50 which are integral with the rim 46 may be friction welded to the rim 46 or may be machined from the disc 42.

The disc 42 comprises a first ring of fibres 52, the individual ceramic fibres 54 extending circumferentially through 360 degrees. The first ring of fibres 52 is arranged substantially at a first radial distance  $R_1$  from the axis of rotation X of the disc 42 and the first ring of fibres 52 is coaxial with the axis of rotation X. The disc 42 comprises a second ring of fibres 56, the individual ceramic fibres 58 extending circumferentially through 360 degrees. The second ring of fibres 56 is arranged substantially at a second radial distance  $R_2$  from the axis of rotation X and the second ring of fibres 56 is coaxial with the axis of rotation X. The second radial distance  $R_2$  is greater than the first radial distance  $R_1$ . In this example the first ring of fibres 52 is arranged in the hub 44 of the disc 42 and the second ring of fibres 56 is arranged in the rim 46 of the disc 42. The volume fraction of fibres in the rings of fibres 52 and 56 is about 30 percent, but other volume fractions may be used.

The second ring of fibres 56 is introduced into the rim 46 of the disc 42 to reduce the density of the rim 44 and hence its weight, but the second ring of fibres 56 is designed to be insufficient on its own to carry the load of the compressor rotor blades 50. The second ring of fibres 56 also reduces the load carrying requirement of the hub 44 of the disc 42 and thus enables the hub 44 to be made smaller. The first ring of fibres 52 is introduced into the hub 44 of the disc 42 to carry the loads on the compressor rotor blades

50 and reduces the density of the hub 44 and hence its weight. The result of using the ceramic fibre reinforcement at the hub 44 and rim 46 of the disc 42 is that both the hub 44 and the rim 46 of the disc are reduced in size, density and weight compared to the conventional solid metal disc.

As an example a ceramic fibre reinforced titanium disc 42 with an outer radius of about 0.5 metres or greater, carrying large, heavy, compressor blades and arranged to operate at about 11000 revolutions per minute (rpm) has a 26 percent reduction in weight compared to the conventional solid titanium metal disc 12, and a 34 percent reduction in weight compared to a ceramic fibre reinforced titanium ring 32.

However, because the free ring radius decreases with increasing speed and decreases with increasing blade loading the ceramic fibre reinforced compressor rotor 40 with a smaller outer diameter than 0.5 metres may be lighter than a conventional solid metal compressor rotor 10, of the same diameter, if the speed of rotation and or blade loads are sufficiently high.

A turbofan gas turbine engine 90, as shown in figure 4, comprises in axial flow series an inlet 92 a fan section 94, a compressor section 96, a combustion section 98, a turbine section 100 and an exhaust 102. The compressor section comprises one or more fibre reinforced discs 42 as described with reference to figure 3.

A fibre reinforced metal rotor 42 as shown in figure 3 is manufactured using preforms as shown in figure 5. A first metal ring 112, or metal disc, is formed and a first annular axially extending groove 114 and a second annular axially extending groove 116 are machined in one axial face 118 of the first metal ring 112. The first and second annular

grooves 114 and 116 are arranged at radial distances of  $R_1$  and  $R_2$  respectively from the axis X of the metal ring 112. The annular grooves 114 and 116 have parallel straight sides which form a rectangular cross-section. A second metal ring 120, or metal disc, is formed and a first annular axially extending projection 122 and a second annular axially extending projection 124 are machined from the second metal ring 120 such they extend from one axial face 126 of the second metal ring 120. The second metal ring 120 is also machined to form four annular grooves 128, 130, 132 and 134 in the face 126 of the second metal ring 120. The grooves 128 and 130 are arranged radially on either side of the first annular projection 122 and the grooves 132 and 134 are arranged radially on either side of the second annular projection 124. The grooves 128, 130, 132 and 134 taper from the axial face 126 to the bases of the annular projections 122 and 124.

Circumferentially extending fibres 56 and 54 are arranged in the first and second annular grooves 114 and 116 respectively. The fibres 54 and 56 may be one or more annular fibre preforms, each annular fibre preform comprising a metal coated fibre which is wound into a planar spiral. A sufficient number of fibres, or annular fibre preforms, are stacked in the annular grooves 114 and 116 to partially fill the annular grooves 114 and 116 to predetermined levels.

The second metal ring 120 is then arranged such that the axial face 126 confronts the axial face 118 of the first metal ring 112, and the axes of the first and second metal rings 112 and 120 are aligned such that the first and second annular projections 122 and 124 on the second metal ring align with the first and second annular grooves 114 and 116 respectively of the first metal ring 112. The second metal



ring 120 is then pushed towards the first metal ring 112 such that the first annular projection 122 enters the first annular groove 114 and the second annular projection 124 enters the second annular groove 116. The second metal ring  
5 120 is further pushed until the axial face 126 of the second metal ring 120 abuts the axial face 118 of the first metal ring 112. The grooves 128, 130, 132 and 134 then form annular chambers between the confronting faces 118 and 126 of the first and second metal rings 112 and 120.

10 The radially inner and outer peripheries of the axial face 118 of the first metal ring 112 are sealed to the radially inner and outer peripheries respectively of the axial face 126 of the second metal ring 120 to form a sealed assembly. The sealing is performed by TIG welding, electron  
15 beam welding, laser welding or other suitable welding process to form outer and inner weld seals 136 and 138 respectively.

The second metal ring is provided with pipes 140 and 142 which extend through holes in the second metal ring 120 and which interconnect to the annular grooves 128 and 132  
20 respectively. The annular projections 122 and 124 are provided with axially extending slots.

The pipes 140 and 142 are connected to vacuum pumps and the sealed assembly is evacuated. The sealed assembly is heated to evaporate any glue used to hold the fibre preforms  
25 in place, and the evaporated glue passes along the slots on the annular projections 122 and 124 into the annular grooves 128 and 132 and through the pipes 140 and 142. The annular projections prevents movement of the metal coated fibres once the glue has been removed.

30 The sealed assembly is then heated to diffusion bonding temperature and isostatic pressure is applied to the sealed assembly, this is known as hot isostatic pressing, and this

results in axial consolidation of the fibres and diffusion bonding of the first metal ring 112 to the second metal ring 120 and diffusion bonding of the metal on the metal coated fibres to the metal on other fibres and to the first and second metal rings 112 and 120. Following hot isostatic pressing the resulting consolidated and diffusion bonded fibre reinforced metal component is machined to produce the shape of the fibre reinforced metal disc 42. This may involve machining blades from the component, or friction welding blades onto the component or machining axially or circumferentially extending slots to receive blade roots.

This method of manufacture is disclosed more fully in our UK patent application No. 9619890.8 filed 24 September 1996, and this should be consulted for more details.

The ceramic fibres may be silicon nitride, silicon carbide, boron, alumina or other suitable fibres.

The metal disc may comprise titanium, titanium aluminide, an alloy of titanium, or any suitable metal, alloy or intermetallic which is capable of being bonded.

The hoop strength of the rings of fibres may be varied by varying the volume fraction of the fibres in the rings of fibres, however 35% is normally used, volume fractions above 35% produce reduced transverse strength.

Although the invention has referred to compressor rotors and discs, the invention is equally applicable to gas turbine engine turbine rotors and discs. The invention is also applicable to other rotors or discs, for example steam turbines etc. The invention is particularly suitable for applications where the fibre reinforced metal rotor has a large diameter and is intended to rotate at high speeds, however the invention is also suitable for other circumstances.

Claims:-

1. A fibre reinforced metal rotor comprising at least two rings of fibres, the fibre reinforced metal rotor having an axis of rotation, a first ring of fibres being arranged substantially at a first radial distance from the axis of rotation, a second ring of fibres being arranged substantially at a second radial distance from the axis of rotation and the second radial distance is greater than the first radial distance.
2. A fibre reinforced metal rotor as claimed in claim 1 wherein the fibre reinforced metal rotor comprises a disc, the disc comprising a hub, a rim and a diaphragm extending radially between the hub and the rim.
3. A fibre reinforced metal rotor as claimed in claim 2 wherein the first ring of fibres is arranged in the hub and the second ring of fibres is arranged in the rim.
4. A fibre reinforced metal rotor as claimed in any of claims 1 to 3 wherein the fibre reinforced metal rotor comprises titanium, titanium aluminide, an alloy of titanium, or any suitable metal, alloy or intermetallic which is capable of being bonded.
5. A fibre reinforced metal rotor as claimed in any of claims 1 to 4 wherein the reinforcing fibres comprise silicon carbide, silicon nitride, boron, alumina or other suitable fibres.
6. A fibre reinforced metal rotor as claimed in any of claims 1 to 5 wherein the fibre reinforced metal rotor has at least one rotor blade.
7. A fibre reinforced metal rotor as claimed in any of claims 1 to 6 wherein the at least one rotor blade is integral with the fibre reinforced metal rotor.

8. A fibre reinforced metal rotor as claimed in any of claims 1 to 6 wherein the at least one rotor blade has a root arranged to fit in at least one axially, or circumferentially, extending groove in the fibre reinforced metal rotor.
9. A fibre reinforced metal rotor as claimed in any of claims 1 to 8 wherein the fibre reinforced metal rotor has an outer radius, the outer radius is at least about 0.5 metres.
10. A fibre reinforced metal rotor substantially as hereinbefore described with reference to and as shown in figure 3 of the accompanying drawings.
11. A gas turbine engine comprising a fibre reinforced metal rotor as claimed in any of claims 1 to 10.

ABSTRACTA FIBRE REINFORCED METAL ROTOR

5 A fibre reinforced metal compressor disc (42) comprises a hub (44), a rim (46) and a diaphragm (48) extending radially between the hub (44) and the rim (46). The fibre reinforced metal compressor disc (40) comprises a first ring of ceramic fibres (52) and a second ring of ceramic fibres (56). The  
10 first ring of fibres (52) is arranged in the hub (44) and the second ring of fibres (56) is arranged in the rim (46) of the disc (42). The rim (46) of the disc (42) carries a plurality of blades (50). This arrangement of the rings of fibres (52,56) minimises the weight of the disc, especially for  
15 large radius discs suitable for carrying large blades and operating at high rotational speeds.

(Figure 3)

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Fig 1

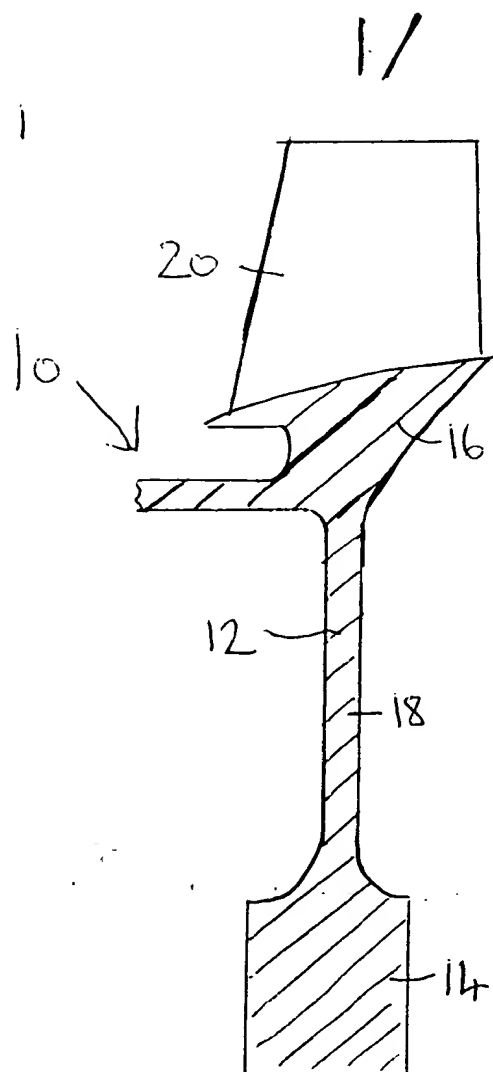
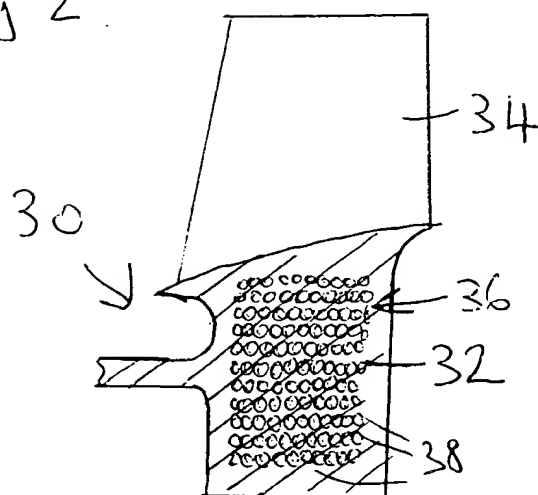


Fig 2



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Fig 3

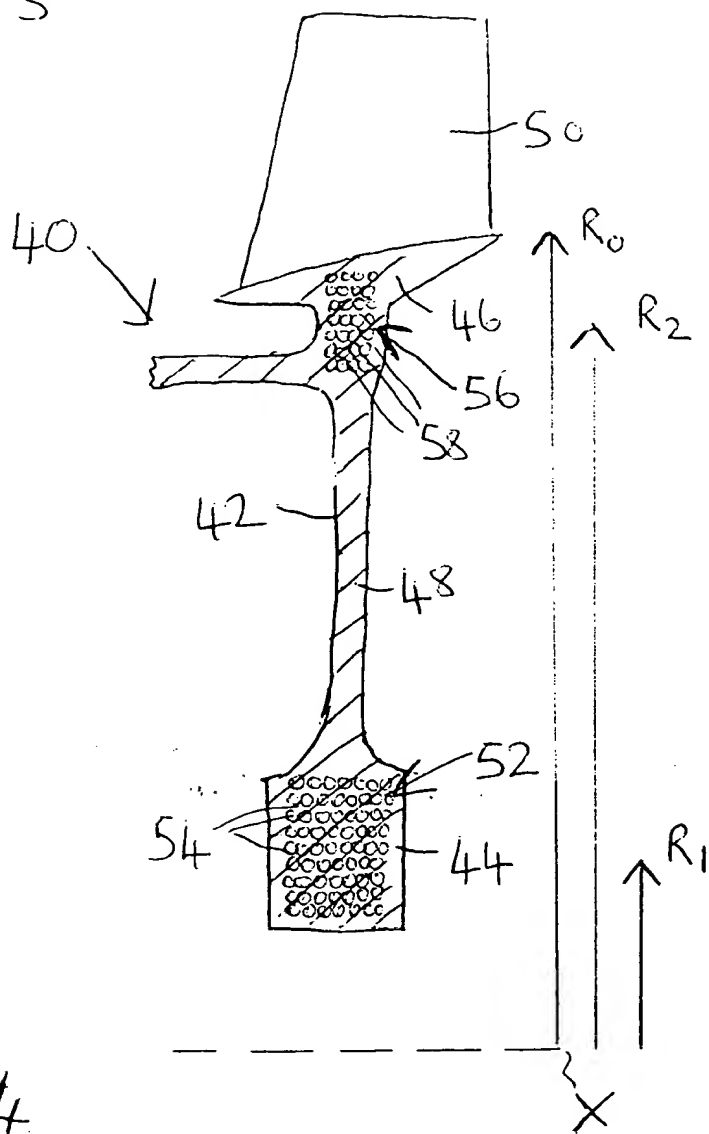
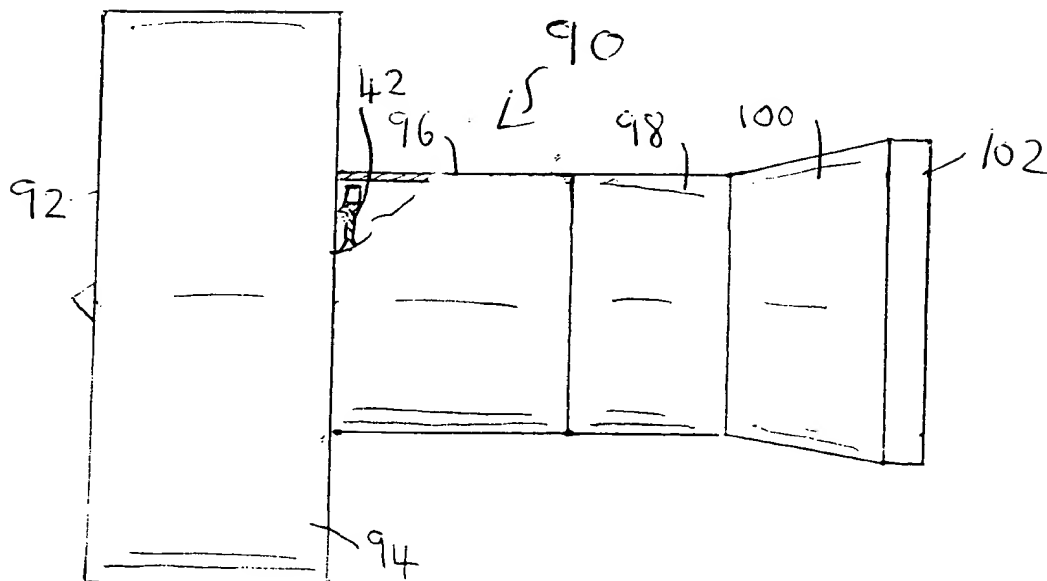


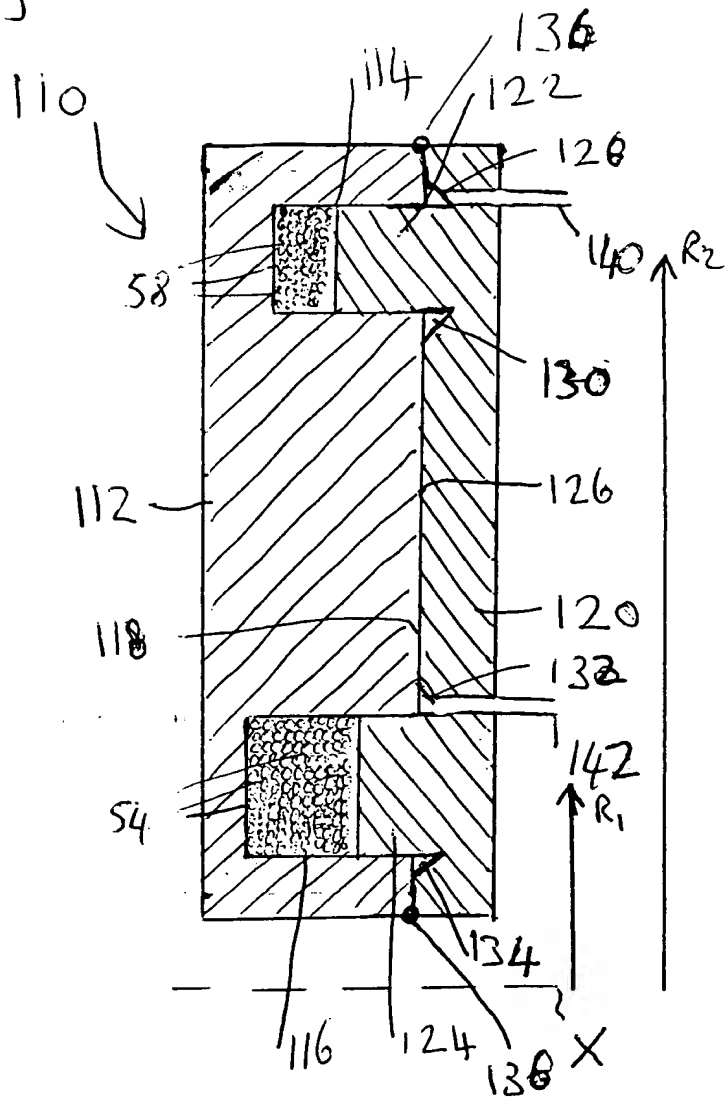
Fig 4



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Fig 5



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14 May 1998

PATENTS ACT 1977

CONDITIONAL PERMIT FOR FILING A PATENT APPLICATION  
OUTSIDE THE UNITED KINGDOM

Application No. GB9711768.3

Filed 3 June 1997

On **16 June 1997** directions were given under Section 22(1) prohibiting publication of information contained in the above-numbered application for defence reasons. The directions are still in force, but the applicant is hereby authorised to apply in **THE UNITED STATES** for grant of a patent in respect of matter contained in the application, subject to the conditions set forth below:-

- (1) The application has been classified by a defence authority of the United Kingdom as **RESTRICTED** and the receiving Government shall be requested to place the corresponding application in secrecy and accord it at least the equivalent security classification.
- (2) The corresponding application shall be abandoned if this action becomes necessary to ensure secrecy.
- (3) All correspondence relating to the corresponding application shall be transmitted solely through officially recognised adequately secure communication channels. All persons in the receiving country required to deal with the patent application there shall have been authorized to have access to such security classified information and be able to provide adequate physical security.
- (4) The applicant shall make available to the receiving Government for defence purposes a copy of the application filed in that country.

This permit applies only to matter disclosed in the United Kingdom application, and it does not authorise the making of an application under the European Patent Convention or the Patent Cooperation Treaty.

for the Comptroller

DP Per 3/77

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